## Module 3c: Flow in Pipes <br> Hazen-Williams Equation

## Hazen-Williams Equation

Based on experimental work

- Used to calculated velocity in a pipe based on the relative roughness and slope of the energy line

$$
V=k C R^{0.68} 3^{0.54}
$$

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## Hazen-Williams Equation

| Type of Pipe | C |
| :--- | :---: |
| Pipes extremely straight and smooth | 140 |
| Pipes very smooth | 130 |
| Smooth wood, smooth masonry | 120 |
| New riveted steel, vitrified clay | 110 |
| Old cast iron, ordinary brick | 100 |
| Old riveted steel | 95 |
| Old iron in bad condition | $60-80$ |

## Hazen-Williams Equation

| Pipe Material | C |
| :--- | :---: |
| New cast iron | 130 |
| 5-year old cast iron | 120 |
| 20-year old cast iron | 100 |
| Average concrete | 130 |
| New welded steel | 120 |
| Asbestos cement | 140 |
| Plastic | 150 |

In: Warren Viessman, Jr. and Mark Hammer. Water Supply and Pollution Control, Sixth Edition. Addison-Wesley. 1998. Table 6-1.

[^0] Table 2-2.

| Hazen-Williams Equation |  |
| :--- | :---: |
| Description of Pipe | Value of C |
| Cast iron | 130 |
| New | 130 |
| 5 years old | 120 |
| 10 years old | 110 |
| 20 years old | $90-100$ |
| 30 years old | $75-90$ |
| Concrete | 120 |
| Cement lined | 140 |
| Welded steel | As for cast iron 5 years older |
| Riveted steel | As for cast iron 10 years older |
| Plastic | 150 |
| Asbestos Cement | 140 |

In: Terence McGhee. Water Supply and Sewerage, Sixth Edition. McGraw-Hill. 1991.

Channel Characteristics: Hydraulic Radius and Wetted Perimeter

- Wetted Perimeter - surface of pipe or channel where fluid is touching (accounts for areas where friction effects are occurring).
- Not used to describe any area that is open to the atmosphere since friction contact with the atmosphere is negligible.



## Hazen-Williams Equation

- For circular pipes flowing full, the Hazen-Williams formula can be restated:

For a circular pipe flowing full:

$$
R=\frac{D}{4}
$$

By Continuity:

$$
Q=V A
$$

## Hazen-Williams Equation

- For circular pipes flowing full, the Hazen-Williams formula can be restated:

Conversion Factor:
$1 \mathrm{ft} 3 / \mathrm{sec}(7.48 \mathrm{gal} / \mathrm{ft} 3)=7.48 \mathrm{gal} / \mathrm{sec}$
$7.48 \mathrm{gal} / \mathrm{sec}(60 \mathrm{sec} / \mathrm{min})=448 \mathrm{gal} / \mathrm{min}$
$448 \mathrm{gal} / \mathrm{min}(60 \mathrm{~min} / \mathrm{hr})(24 \mathrm{hr} /$ day $)=646,272 \mathrm{gal} /$ day $646,272 \mathrm{gal} /$ day $\cong 0.646 \mathrm{million} \mathrm{gal} /$ day
Conversion Factor $=0.646 \mathrm{MGD} / c f s$

## Hazen-Williams Equation

- Substituting into Hazen-Williams:

$$
\begin{aligned}
& Q=0.432 C D^{2.63} S^{0.54}\left[\text { units of } \mathrm{ft}^{3} / \mathrm{sec}\right] \\
& Q=0.432 C D^{2.63} S^{0.54}(0.646 M G D / c f s) \\
& Q=0.279 C D^{2.63} S^{0.54}
\end{aligned}
$$

$$
\begin{array}{ll}
\text { Where } & \mathrm{Q}=\text { flow (MGD) } \\
& \mathrm{D}=\text { diameter }(\mathrm{ft})
\end{array}
$$

## Hazen-Williams Equation

- Substituting into Hazen-Williams:
$V[f t / \mathrm{sec}]=1.318 C R 0.63 S 0.54$
$V[f t / \mathrm{sec}] A\left[f t^{2}\right]=1.318 A C R 0.63 S 0.54$
$Q\left[f t^{3} / \mathrm{sec}\right]=1.318 \frac{\pi}{4} D^{2} C\left(\frac{D}{4}\right)^{0.63} S^{0.54}$
$Q=1.035 D^{2}\left(\frac{D}{4}\right)^{0.63} C S^{0.54}$
$Q=\left(\frac{1.035}{4^{0.63}}\right) C D^{2.63} S^{0.54}$
$Q=0.432 C D^{2.63} S^{0.54}\left[\right.$ units of $\mathrm{ft}^{3} / \mathrm{sec}$ and ft$]$


## Hazen-Williams Equation

- For SI units, the Hazen-Williams equation for pipes flowing full:

$$
Q=0.278 C D^{2.63} S^{0.54}
$$

Where

$$
\begin{aligned}
& \mathrm{Q}=\text { flow }\left(\mathrm{m}^{3} / \mathrm{sec}\right) \\
& \mathrm{D}=\text { pipe diameter }(\mathrm{m})
\end{aligned}
$$



## Hazen-Williams Equation

## Example:

- Determine the head loss in a $1000-\mathrm{m}$ pipeline with a diameter of 500 mm that is discharging $0.25 \mathrm{~m}^{3} / \mathrm{sec}$. Assume that the Hazen-Williams coefficient for the pipe equals 130 .

Given: $\mathrm{L}=1000 \mathrm{~m}$
$\mathrm{D}=0.5 \mathrm{~m}$
$\mathrm{Q}=0.25 \mathrm{~m}^{3} / \mathrm{sec}$
$\mathrm{C}=130$

## Hazen-Williams Equation

- Using the Hazen-Williams equation for flow:

$$
Q=0.278 C D^{2.63} S^{0.54}
$$

- By definition:

$$
S=\frac{h_{f}}{L}
$$

- Substituting:

$$
Q=0.278 C D^{2.63}\left(\frac{h_{f}}{L}\right)^{0.54}
$$

## Hazen-Williams Equation

- Solving for $\mathrm{h}_{\mathrm{f}}$ :

$$
\begin{aligned}
& \frac{Q}{0.278 C D^{2.63}}=\left(\frac{h_{f}}{L}\right)^{0.54} \\
& \frac{h_{f}}{L}=\left(\frac{Q}{0.278 C D^{2.63}}\right)^{1 / 0.54} \\
& h_{f}=L\left(\frac{Q}{0.278 C D^{2.63}}\right)^{1 / 0.54} \\
& \text { Substituting : } \\
& h_{f}=(1000 m)\left(\frac{\left(0.25 m^{3} / \mathrm{sec}\right)}{0.278(130)(0.5 m)^{2.63}}\right)^{1.85} \\
& h_{f}=2.94 m
\end{aligned}
$$

## Hazen-Williams Equation

## Example:

- A 14 -inch diameter schedule 80 pipe has an inside diameter of 12.5 inches ( 317.5 mm ). What is the friction factor $f$ if the pipe is flowing full and the allowable head loss is 3.5 m in a length of 200 m ? Use Hazen-Williams equation to calculate velocity.

$$
V=k C R^{0.63} S^{0.54}
$$

## Hazen-Williams Equation

- Substituting into the Hazen-William equation:
- For SI units, k=0.849

$$
\begin{aligned}
& V=(0.849) C R^{0.63} S^{0.54} \\
& V=(0.849)(120)(0.079375 m)^{0.63}(0.0175)^{0.54} \\
& V=2.32 \mathrm{~m} / \mathrm{sec}
\end{aligned}
$$

- Calculate a Reynolds number based on this velocity:

$$
\begin{aligned}
& \operatorname{Re}=\frac{V D}{v}=\frac{2.32 \mathrm{~m} / \mathrm{sec}(0.3175 \mathrm{~m})}{1.003 \times 10^{-6} \mathrm{~m}^{2} / \mathrm{sec}} \\
& \operatorname{Re}=7.3 \times 10^{5}
\end{aligned}
$$

## Hazen-Williams Equation

- Assume that the pipe is cast-iron $\Rightarrow \mathrm{C}=120$
- Calculate the slope of the energy gradient:

$$
\begin{aligned}
& S=\frac{h_{f}}{L}=\frac{3.5 m}{200 m} \\
& S=0.0175
\end{aligned}
$$

- Calculate the hydraulic radius, R , for pipe flowing full:

$$
R=\frac{D}{4}=\frac{0.3175 \mathrm{~m}}{4}=0.079375 \mathrm{~m}
$$

Refer to Moody Diagram


Reading from the Moody diagram (since this is based on a previous problem, $\varepsilon / d$ has already been calculated and is 0.000012 ):

$$
f=0.0125
$$

## Hazen-Williams Equation

To correct for C factors not equal to 100 when using the HazenWilliams nomogram:

- Given flow and diameter, find $\mathrm{S}_{100}$ from the nomogram:

$$
S_{C}=S_{100}\left(\frac{100}{C}\right)^{1.85}
$$

- Given flow and slope, find $\mathrm{D}_{100}$ from the nomogram:

$$
D_{C}=D_{100}\left(\frac{100}{C}\right)^{0.38}
$$

- Given diameter and slope, find flow from nomogram:

$$
Q_{C}=Q_{100}\left(\frac{C}{100}\right)
$$

Example (using the nomogram and the conversions):

- A schedule 80 pipe has an inside diameter of 12.5 inches ( 317.5 mm ). What is the velocity if the pipe is flowing full and the allowable head loss is 3.5 m in a length of 200 m? Use Hazen-William equation to calculate velocity. Assume C = 120 .
- Given: $\mathrm{D}=12.5$ inches

$$
\mathrm{H}_{\mathrm{L}}=3.5 \mathrm{~m}
$$

$$
\mathrm{L}=200 \mathrm{~m}
$$

## Hazen-Williams Equation

- Calculate slope of energy line.

$$
\begin{aligned}
& S=\frac{H_{L}}{L}=\frac{3.5 m}{200 m} \\
& S=0.0175
\end{aligned}
$$

- To use the nomogram, need slope as feet/1000 feet.

$$
\begin{aligned}
& S=0.0175 f t / f t\left(\frac{1000 f t}{1000 f t}\right) \\
& S=17.5 f t / 1000 f t
\end{aligned}
$$

## Hazen-Williams Equation

## Hazen-Williams Equation

- Modifying based on flow conversion (divide both sides by area) and substituting:

$$
\begin{aligned}
& Q_{C}=Q_{100}\left(\frac{C}{100}\right) \\
& V=\frac{Q}{A} \\
& V_{C}=\frac{Q_{C}}{A}=Q_{100}\left(\frac{C}{100}\right)=\frac{V_{100}}{A}\left(\frac{C}{100}\right) \\
& V_{C}=V_{100}\left(\frac{C}{100}\right) \\
& V_{C}=(1.83 \mathrm{~m} / \mathrm{sec})\left(\frac{120}{100}\right) \\
& V_{120}=2.2 \mathrm{~m} / \mathrm{sec}
\end{aligned}
$$

Example:

- Determine the head loss in a $46-\mathrm{cm}$ concrete pipe with an average velocity of $1.0 \mathrm{~m} / \mathrm{sec}$ and a length of 30 m .
- Using Hazen-Williams equation:

$$
V=k C R^{0.63} S^{0.54}
$$

- $\quad$ Since in SI units, $\mathrm{k}=0.849$
- For a pipe flowing full:

$$
\begin{aligned}
& R=\frac{D}{4}=\frac{0.46 \mathrm{~m}}{4} \\
& R=0.115 \mathrm{~m}
\end{aligned}
$$

## Hazen-Williams Equation

- By definition:

Slope of energy line $=$ Head Loss/Length of Pipe
Or

Head Loss $=\mathrm{h}_{\mathrm{L}}=($ Slope $)$ (Pipe Length)

- Let C = 130 (concrete pipe $\Rightarrow$ use average of 120 - 140)
- Solve Hazen-Williams for Slope:

$$
\begin{gathered}
V=k C R^{0.63} S^{0.54} \\
S^{0.54}=\frac{V}{k C R^{0.63}} \\
S=\left(\frac{V}{k C R^{0.63}}\right)^{1 / 0.54}
\end{gathered}
$$

## Hazen-Williams Equation

## Hazen-Williams Equation

Example:

- Find the discharge from a full-flowing cast iron pipe 24 in. in diameter having a slope of 0.004 .
- Assume: 5-year old cast iron $\Rightarrow \mathrm{C}=120$
- Using Hazen-Williams:

$$
\mathrm{Q}=0.279 C D^{2.63} \mathrm{~S}^{0.54}
$$

- The flow will be given in MGD, but it is needed in $\mathrm{ft}^{3} / \mathrm{sec}$.
- From earlier, conversion factor for MGD to cfs is: $1 \mathrm{ft}^{3} / \mathrm{sec}=0.646 \mathrm{MGD}$

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## Hazen-Williams Equation

- Modify Hazen-Williams:

$$
\begin{aligned}
& Q=0.279 C D^{2.63} S^{0.54}\left(\frac{1 f t^{3} / \mathrm{sec}}{0.646 M G D}\right) M G D \\
& Q=0.432 C D^{2.63} S^{0.54}
\end{aligned}
$$

for flow in $\mathrm{ft}^{3} / \mathrm{sec}$

- Substituting:

$$
\begin{aligned}
& Q=0.432(120)\left(\frac{24 i n}{12 i n / f t}\right)^{2.63}(0.004)^{0.54} \\
& Q=16.27 c f s
\end{aligned}
$$


[^0]:    n: Metcalf \& Eddy, Inc. and George Tchobanoglous. Wastewater Engineering: Collection and Pumping of Wastewater. McGraw-Hill, Inc. 1981.

